



EN 1992

2nd generation of Eurocode 2 on concrete structures



Design of concrete



DURABILITY IN CHAPTER 6

- 1. A small change in the definition of the XC2
 - 1. The Exposure classes are incorporated as "environmental actions"
- 2. Cover depths in fuction of the ERC's and the XC's and calibrated with durability models
 - 1. There will be an EN 206-100 for verification of durability
 - 2. The previous methodology will be allowed
 - 3. It is introduced a new LIMIT state in addition to depassivation
 - Condition or Deterioration LS
 - 2. In includes a corrosion propagation period
 - 1. 50 μm of homogeneous attack
 - 2. 500 μm of localized attack
- 3. Cover depths for stainless steel bars.
- 4. Annex I Assessment of existing structures

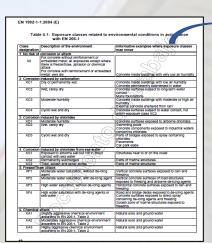


PREVIOUS METHODOLOGY FOR DURABILITY DESIGN AND INTRODUCTION OF ERC'S

Exposure classes + Structural classes



cover depths



Та	le 4.4N:	Values of minimum cover, c _{min,dur} , requirements with regard to durability for
		reinforcement steel in accordance with EN 10080.

Environment of c _{min,dur} (mm)											
Structural	posui										
Class		XC1	XC2 / XC3	XC4	X	D1 / XS1	XD2 / XS2	XD3 / XS3	3		
S1	10	10	10	15		20	25 (/ />	√ / 30			
S2	10		15	20		25	30	35	\neg		
S3	10	10	20	25		30	35	40	\neg		
S4	10	15	25	30		35 <	40	45			
S5	15	20		35		40	45	50			
S6	20	25	35	40		45	50	55	7		

Table 4.5N: Values of minimum cover, cmin.dur. rements with regard to durability for prestressing steel

Environmenta	Environmental Requirement for c _{min,dur} (mm)										
Structural Exposure Class according to Table 4.1											
Class	XD2 / XS2	XD3/XS	3								
S1	10	15	20	25		_30	35	40			
S2	10	15	25	30		/35	2	45			
S3	10	20	30	/35	~	40	45	50			
S4	10	25	35	40		45	50	55			
S5	15	30	40	45		50	55	60			
S6	20	35	45	50	17	55	60	6			

(6) The concrete cover should be increased by the additive safety element Δc_{dut.y}.

Note: The value of $\Delta c_{dur, r}$ for use in a Country may be found in its National Annex. The recommended value is

(7) Where stainless steel is used or where other special measures have been taken, the minimum cover may be reduced by $\Delta c_{dur.st}$. For such situations the effects on all relevant

					EXPO	SURE CL	ASSES					
	No	Ca	rbonatio	on induc	ed		Chloride induced corrosion					
	risk		corre	osion		9	ea wate	r	Chlor	ide othe	er tan	
									fror	n sea w	ater	
	X0	XC1	XC2	XC3	XC4	XS1	XS2	XS3	XD1	XD2	XD3	
a/c	-	0.65	0.60	0.55	0.50	0.50	0.45	0.45	0.55	0.55	0.45	
strength	C12/	C20/	C25/	C30/	C30/	C30/	C35/	C35/	C30/	C30/	C35/	
	15	25	30	37	37	37	45	45	37	37	45	
cement	-	260	280	280	300	300	320	340	300	320	340	
Cover	10	15	25	25	30	35	40	45	35	40	45	
depth												
S4(mm)												

THE STRUCTURAL **CLASSES ARE** SUBSTITUTED BY THE **EXPOSURE RESISTANCE CLASSES (ERC)**

COVER DEPTHS IN FUNCTION OF ERC's mínimum cover Depth

carbonation

prEN 1992-1-1:2020 (E)

Table $\sigma_{\bf k}^{\bf k}({
m NDP})$ — Minimum concrete cover $c_{
m min,dur}$ for carbon steel — Carbonation

			Expo	sure class	(carbonat	tion)				
EDC	X	C 1	XC2		XC3		XC4			
ERC	Design service life (years)									
	50	100	50	100	50	100	50	100		
XRC 0,5	10	10	10	10	10	10	10	10		
XRC 1	10	10	10	10	10	15	10	15		
XRC 2	10	15	10	15	15	25	15	25		
XRC 3	10	15	15	20	20	30	20	30		
XRC 4	10	20	15	25	25	35	25	40		
XRC 5	15	25	20	30	25	45	30	45		
XRC 6	15	25	25	35	35	55	40	55		
XRC 7	15	30	25	40	40	60	45	60		

NOTE 1 The designation of XRC classes for resistance against corrosion induced by carbonation is derived from the carbonation depth [mm] (characteristic value 90 % fractile) assumed to be obtained after 50 years under reference conditions (400 ppm CO2 in a constant 65 %-RH environment and at 20 °C). XRC has the dimension of a carbonation rate $[mm/\sqrt{(years)}]$

NOTE 2 The recommended minimum concrete cover values $c_{min,dur}$ assume execution and curing according to EN 13670 with at least Execution Class 2 and Curing Class 2.

NOTE 3 The minimum covers can be increased by an additional safety element $\Delta c_{dur,v}$ considering special requirements (e.g. more extreme environmental conditions).

chlorides

Table 6.4(NDP) — Minimum concrete cover $c_{min,dur}$ for carbon steel — Chlorides

						Expos	ure cla	ss (chlo	rides)				
ERC		XS	S1	XS2		XS	XS3		XD1		XD2		03
EKC		Design service life (years						Design service life (years)					
		0	100	50	100	50	100	50	100	50	100	50	100
XRDS 0,5	П	:0	20	20	30	30	40	20	20	20	30	30	40
XRDS 1		20	25	25	35	35	45	20	25	25	35	35	45
XRDS 1,5		25	30	30	40	40	50	25	30	30	40	40	50
XRDS 2		25	30	35	45	45	55	25	30	35	45	45	55
XRDS 3		30	35	40	50	55	65	30	35	40	50	55	65
XRDS 4		30	40	50	60	60	80	30	40	50	60	60	80
XRDS 5		35	45	60	70	70	_	35	45	60	70	70	_
XRDS 6		Ю	50	65	80	_	_	40	50	65	80	_	_
XRDS 8		ŀ5	55	75	_	_	_	45	55	75	_	_	_
XRDS 10		50	65	80	_	_	_	50	65	80	_	_	_

signation of XRDS classes for resistance against corrosion induced by chloride ingress is derived from the depth of chlorides penetration [mm] (characteristic value 90 % fractile), corres-ponding to a reference chlorides concentration (0,6 % by mass of bindercement + type II additions), assumed to be obtained after 50 years on a concrete exposed to one-sided penetration of reference seawater (30 g/l NaCl) at 20 °C. XRDS has the dimension of a diffusion coefficient $[10^{-13} \text{ m}^2/\text{s}]$.

NOTE 2 The recommended minimum concrete cover values cmin,dur assume execution and curing according to EN 13670 with at least Execution Class 2 and Curing Class 2.

NOTE 3 The minimum covers can be increased by an additional safety element Δcdury considering special requirements (e. g. more extreme environmental conditions).

(2) For temporary structures or for structures with a design service life of 30 years or less, cmindur for a design service life of 50 years according to Table 6.3(NDP) and Table 6.4(NDP) may be reduced by

NOTE 3 The reduction of the cover is $-\Delta c_{\min,30} \le 5$ mm unless a National Annex gives a different value.

STAINLESS STEEL

Q.4 Minimum cover for durability

(1) For durability design with stainless steel reinforcement, Stainless Steel Resistance Classes SSRC are defined in Table 0.2.

For an alternative approach to design cover for durability without use of Exposure Resistance Classes NOTE (ERC) see Annex P.

Table Q.2. Classification of corrosion resistance of stainless steel dependent on the Pitting Resistance Eqvivalent PRE

Stainless	Pitting		Informati	ve example	s EN 10088-1
steel Resistance Class	Resistance Equivalent PREª	Description	Ferritic	Duplex	Austenitic
SSRC0	0 to 9	Carbon steel reinforcement	-	-	-
SSRC1	10 to 16	Chromium steels	1.4003	-	_
SSRC2	17 to 22	Chromium Nickel steels	-	1.4482	1.4301 1.4307
SSRC3	23 to 30	Chromium Nickel steels with Molybdenum	-	1.4362	1.4401 1.4404 1.4571
SSRC4	≥ 31	Steels with increased content of Chromium and Molybdenum	-	1.4462	1.4529

Calculation of the Pitting Resistance Equivalent: PRE = $Cr + 3.3 \cdot Mo + n \cdot N$; Cr, Mo and N in M.- %. With: n=0 for ferritic steels, n=16 for Duplex steels and n=30 for austenitic steels.

Table 0.3(NDP) — Minimum concrete cover contrato stainless steel reinforcement

Exposure	Exposure	Stainless steel resistance classa							
Class	resistance class ERC	SSRC1	SSRC2	SSRC3	SSRC4				
XC1	< VDC0	0	0	0	0				
XC2	≤ XRC9	0	0	0	0				
VOO	≤ XRC5	0	0	0	0				
XC3	≤ XRC9	15	0	0	0				
VO4	≤ XRC5	15	0	0	0				
XC4	≤ XRC9	20	0	0	0				
	≤ XRDS1,5	20	15	0	0				
XD1, XS1	≤ XRDS3,5	30	20	15	0				
	≤ XRDS5,5	35	25	20	0				
	≤ XRDS1,5	35	25	20	0				
XD2, XD3, XS2, XS3	≤ XRDS3,5	45	35	25	15				
102, 100	≤ XRDS5,5	55	45	35	25				

NOTE 1 The tabulated cover values apply or a design service life of 50 years unless a National Annex excludes

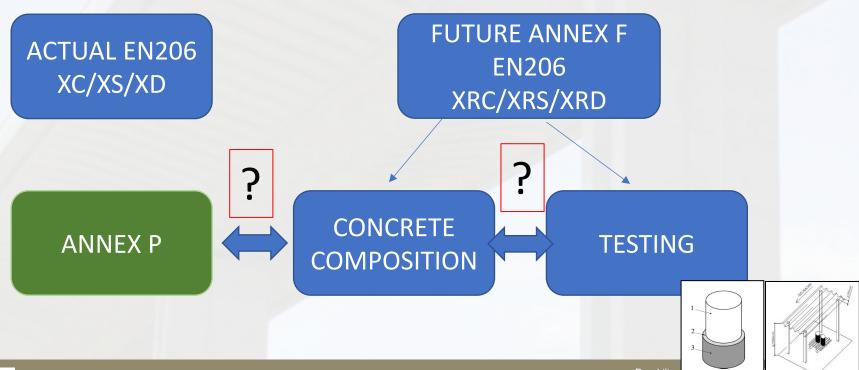
NOTE 2 For a design service life of 100 years cmin,dur in Table Q.3(NDP) should be increased by +10 mm for all ERC classes unless a National Annex excludes some classes or gives other values.

NOTE 3 In case of combined action of carbonation and chloride induced corrosion, cmin,dur in Table Q.3(NDP) should be increased by 20 mm or a higher stainless steel resistance class should be chosen unless a National Annex gives other values.



For stainless steel corrosion resistance classes see Table Q.2.

THREE (INDEPENDENT) ROUTES FOR VERIFICATION OF DURABILITY (to use the cover depths)







DEFINITION of ERC EN-206-100

- NOTE 1: The designation of classes for resistance against corrosion induced by carbonation (XRC) is derived from the carbonation depth in mm (characteristic value 90 % fractile) assumed to be obtained after 50 years under reference conditions (400 ppm CO2 in a constant 65 % RH environment and at 20°C). XRC has the dimension of a carbonation rate (mm / sqrt(years)).
- NOTE 2: The designation of classes for resistance against corrosion induced by chloride ingress (XRDS) is derived from the depth of chlorides penetration in mm (characteristic value 90 % fractile), corresponding to a reference chlorides concentration (0.6 % by mass of cement + type II additions), assumed to be obtained after **50 years** on a concrete exposed to one-sided penetration of reference seawater (30 g/l NaCl) at 20°C. XRDS has the dimension of a diffusion coefficient (10-13 m²/s).



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Table 63 (NDP) — Minimum concrete cover $c_{
m min,dur}$ for carbon steel — Carbonation

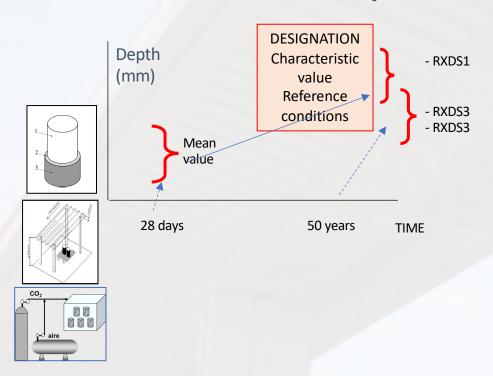
			Expo	sure class	(carbonat	tion)				
	X	C 1	X	XC2		XC3		C4		
ERC	Design service life (years)									
	50	100	50	100	50	100	50	100		
XRC 0,5	10	10	10	10	10	10	10	10		
XRC 1	10	10	10	10	10	15	10	15		
XRC 2	10	15	10	15	15	25	15	25		
XRC 3	10	15	15	20	20	30	20	30		
XRC 4	10	20	15	25	25	35	25	40		
XRC 5	15	25	20	30	25	45	30	45		
XRC 6	15	25	25	35	35	55	40	55		
XRC 7	15	30	25	40	40	60	45	60		

NOTE 1 The designation of XRC classes for resistance against corrosion induced by carbonation is derived from the carbonation depth [mm] (characteristic value 90 % fractile) assumed to be obtained after 50 years under reference conditions (400 ppm CO2 in a constant 65 %-RH environment and at 20 °C). XRC has the dimension of a carbonation rate $[mm/\sqrt{(years)}]$.

NOTE 2 The recommended minimum concrete cover values $c_{\min, dur}$ assume execution and curing according to EN 13670 with at least Execution Class 2 and Curing Class 2.

NOTE 3 The minimum covers can be increased by an additional safety element $\Delta c_{dux,y}$ considering special requirements (e.g. more extreme environmental conditions).

VERIFICATION BY TESTING STARTING FROM THE ITT the mean value is extrapolated to fulfil the cover depth (90%)



From reference conditions to each XC

The test will be in standard conditions



7 % (Beta= 1.5) probability of failure

VERIFICATION BY COMPOSITIONwith annex F of EN 206

		EXPOSURE CLASSES										
/	No	Ca	rbonatio	on induc	ed	Chloride induced corrosion						
	risk		corre	osion		S	ea wate	r	Chlor	Chloride other tan		
									fror	n sea wa	ater	
	X0	XC1	XC2	XC3	XC4	XS1	XS2	XS3	XD1	XD2	XD3	
a/c	-	0.65	0.60	0.55	0.50	0.50	0.45	0.45	0.55	0.55	0.45	
strength	C12/	C20/	C25/	C30/	C30/	C30/	C35/	C35/	C30/	C30/	C35/	
	15	25	30	37	37	37	45	45	37	37	45	
cement	1	260	280	280	300	300	320	340	300	320	340	
Cover	10	15	25	25	30	35	40	45	35	40	45	
depth												
S4(mm)												

(Annex P of EC2)

	Variant 1: New	design	Variant 2:	Current design	
Design step		DC.			
Exposure classes XC, XD, XS, XF, XA, XM	6.3 Environment			vithout ERC	
related to environmental conditions	0.0 Environmen	ин схрозите с	onulions		
	6.3.3, Table 6.1		sses X		
Exposure resistance classes XCR, XRDS, XRF		esistance	-		
related to concrete resistance against corrosion	Classes (ERC)				
or abrasion attacks					
Minimum concrete strength	Depending on n mixes in EN 206			g on current nixes in EN 206 or	
	new Annex F	OF NAD,	NAD. Ann		
	IICW / WILLOW I		TV/CD, / TITE	CX I,	
			P.3 Indicat	tive strength classes	
			for durabili	ity	
Minimum cover cmin	6.5.2.1 General:				
	Cmin = max {Cmin,		A.C	10 mm)	
Minimum cover cmin,dur for durability	Cmin,dur dependin			ending on :	
,		•			
	- XC,	XD, XS and	-	XC, XD, XS and	
	_				
		osure sistance	-	Structural class S and	
		ss XRC.		3 anu	
		DS and	_	design service life	
				50 y or 100 y	
		ign service			
	life	50 y or 100 y			
	6.5.2.2 Minimum	o cover for	D 2 Minim	um cover for	
	durability – carb			carbon, stainless	
	prestressing ste			essing steel	
	Q.2 Minimum co				
Minimum cover cmin,b for bond	durability – stain 6.5.2.3 Minimun		<u>l</u>		
Allowance in design for deviation ∆cdev	6.5.3 Allowance			ble 6.7(NDP)	
Nominal cover cnom	6.5.1 Nominal o			DIO C.I (IIDI)	
Description of concrete durability (examples):	C35/45, XRC2,			C4, XD3, XF2, XA2,	
	XRF, XA2, XM1		XM1		
	c _{min} = 50 mm		<i>c</i> _{min} = 50 n	nm	
	c _{nom} = 60 mm		C _{nom} = 60	mm	

ANNEX I Assessment Existing Structures

Limited to non deteriorated with some comments on deteriorated structures



Assessment of Existing Structures

I.1 Use of this annex

(1) This informative annex supplements provisions in this Eurocode for the assessment of existing structures in plain, reinforced and prestressed concrete. Annex I covers also the assessment of the retained parts of existing concrete structures, that are being modified, extended, strengthened or retrofitted, in case of projects where new structural members are to be combined with retained parts of existing concrete structures.

I.2 Scope and field of application

- This informative annex covers:
- additional rules for materials and system not defined in Clause 5 (e.g. plain bars);
- additional rules for assessing existing structures where detailing does not comply
- with the provisions in Clauses 11 and 12:
- additional rules for anchorage of plain bars;
- considerations for deterioration of existing structures.

L3 General

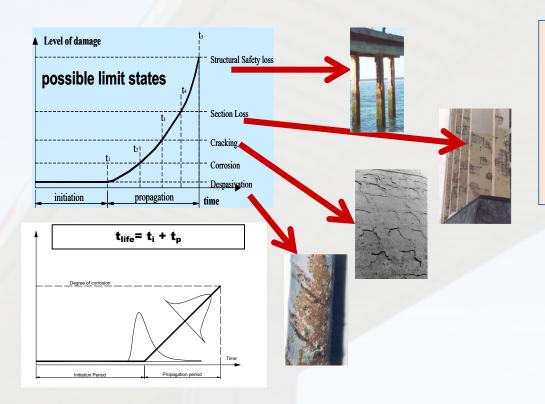
Unless noted otherwise, in Annex I all section/sub-section numbers and titles are similar as the relevant of the main part of this Eurocode. The prefix 'I' is added to clauses numbers to distinguish content that pertain to assessment of existing concrete structures. Annex I contains only sections/subsections of the main part of this Eurocode that include specific clauses for the assessment of existing concrete structures.

- (1) All clauses of this Eurocode are generally applicable to the assessment of existing concrete structures, unless substituted by the provisions given in Annex I.
- (2) Annex I does not provide predictive methods for estimating deterioration rates associated with the various deterioration mechanisms for concrete structures. These should be undertaken using methods specified by the relevant authority or, where not specified, as agreed for a specific assessment by the relevant parties.
- (3) Design values determined in accordance with this Eurocode may be interpreted as assessment values for the purpose of Annex I.
- (4) The following assumptions apply for the assessment of existing concrete structures:
- Reasonable skill and care appropriate to the circumstances is exercised in the assessment, based on the knowledge and good practice generally available at the time the structure is assessed.
- The assessment of the structure is made by appropriately qualified and experienced personnel.





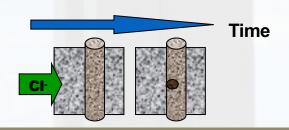
NEW LIMIT STATE (the same in MC2020)



The reason is that in practice the depassivation onset CANNOT BE

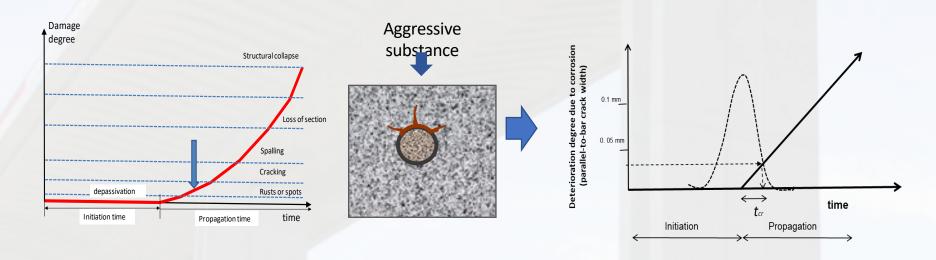
VERIFIED unless permanente sensors are used

CEN does not accept requirements that are not verifiable



END OF SERVICE LIFE

Corrosion propagation is part of the service life until a corrosion depth of 50 μ m (general corrosion) or 500 μ m (localized corrosion with a probability of failure of 7-8% (β = 1.5)



BACKGROUND DOCUMENT EXPLAINING THE CALCULATION OF THE NEW LS AND THE COVER DEPTHS

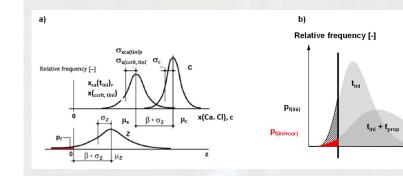
Background Document for prEN1992-1-1:2020 D7 clause 6 - Durability

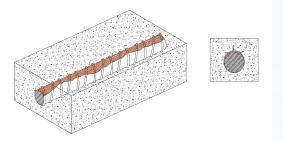
List of content, updated 2021-03-04

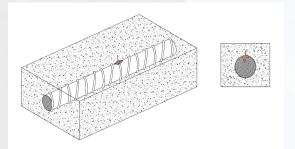
Only main sections listed

(The author/-s of each section and the current TG10 doc N are indicated in parentheses.)

- 1 Introduction
- 1.1 Scope (FT, N335)
- 1.2 Definitions (FT, N335)
- 1.3 Process scheme for performance-based specification (SGD, N329)
- 2 Models for carbonation induced corrosion XRC
- 2.1 Full probabilistic approach I (SGD, N332)
- 2.2 Full probabilistic approach II (DIL/CA, N336)
- 2.3 Deterministic approach using margins and characteristic values (FT, N318b)
- 2.4 Simplified calculations and comparisons (CVN, N337)
- 2.5 Comparisons of XRC models (SGD, FT, CVN, N333)
- 2.6 Covers for XRC (SGD, FT, CA, N333)
- 3 Models for chloride induced corrosion XRDS
 - 3.1 Full probabilistic approach I (SGD, N325)
 - 3.2 Full probabilistic approach II (DIL/CA, N338)
 - 3.3 Deterministic approach using margins and characteristic values (FT. N318c)
 - 3.4 Simplified calculations (CVN, N339)
 - 3.5 Comparisons of XRDS models (SGD, FT, CVN, CA, DIL, N334)
 - 3.6 Covers for XRDS (SGD, FT, CVN, CA, DIL, N334)
- 4 Covers to prestressing steel, to stainless steel and to soil
- 4.1 Prestressing steel (MH, CA, FT, SGD, N340)
- 4.2 Stainless steel (FH, N3XX (N309 updated))
- 4.3 Soil (CE, pending)
- 4.4 Cover to bored piles and diaphragm walls (FF, N298)
- 5 Allowance in design for deviation (FF, N317)









Limit state definition

$$t_{L} = t_{i} + t_{p}$$

- $t_1 = 50$ yrs for tables
- t_p = Propagation time required to achieve 50μm / 500μm under exposure
- t_i = Required initiation time
- Modelling:

$$X_{c} = \sqrt{2 \cdot k_{e} \cdot k_{c} \cdot \frac{D_{Co2}}{a}} \left(\frac{t_{0}}{t}\right)^{w} = \sqrt{\frac{2 \cdot k_{e} \cdot k_{c}}{R_{carb}}} \left(\frac{t_{0}}{t}\right)^{w}$$

$$\mathbf{X_{c} = V_{CO2} \cdot t} \frac{(1-2w)}{2} \qquad \mathbf{V_{Co2} = \sqrt{\frac{2 \cdot \mathbf{k_e} \cdot \mathbf{k_c}}{R_{carb}}}} \left(t_0\right)^{w}$$

$$V_{Co2} = \sqrt{\frac{2 \cdot k_e \cdot k_c}{R_{carb}}} \left(t_0 \right)^w$$

$$t_{desp} = \left(\frac{c}{v_{CO2}}\right)^{\frac{2}{(1.-2w)}}$$

$$Conc(x,t) := \frac{\mathbf{C_0}}{\mathbf{C_0}} + \left(\mathbf{C_S} - \mathbf{C_0}\right) \cdot \left(1 - erf\left(\frac{x - \Delta x}{2 \cdot \sqrt{D_{app}(t) \cdot t}}\right)\right) \qquad D_{app}(t) = D(t_0) \cdot \left(\frac{t_0}{t}\right)^n$$

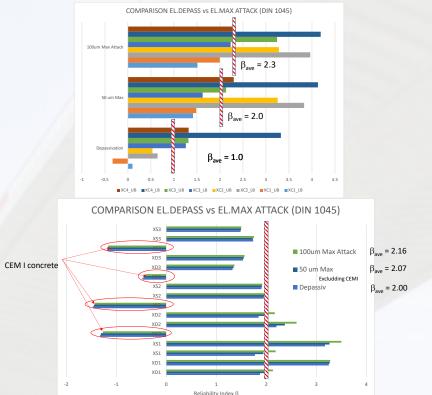
$$V(t) = \text{erf}^{-1}(1-\xi) \bigg[2 \sqrt{D \big(t_0\big) \cdot \big(t_0\big)^n}$$

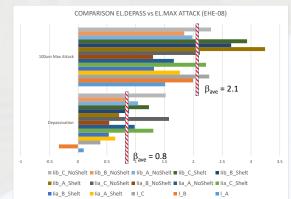
$$t_{\text{dep}} = \left(\frac{C - \Delta x}{V_{\text{cl}}(t)}\right)^{\frac{2}{1-n}}$$

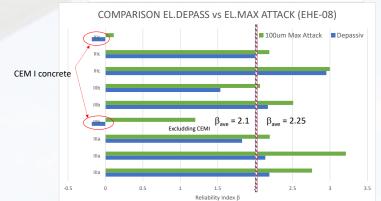
$$D_{app}(t) = D(t_0) \cdot \left(\frac{t_0}{t}\right)^n$$

$$\xi = \frac{C_{cr} - C_0}{C_s - C_0}$$

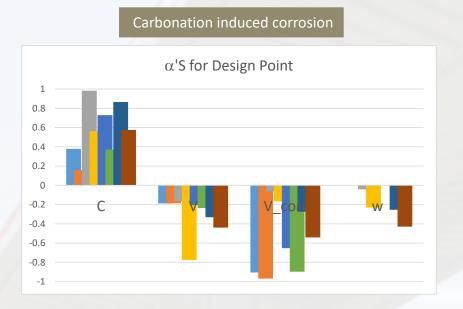
Autocalibration procedure (β_t)

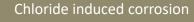






• Autocalibration procedure (Sensitivity factors) α_i







Note: α > 0 "resistance" Variable α < 0 "action" Variable

Service life propagation time uncoupling

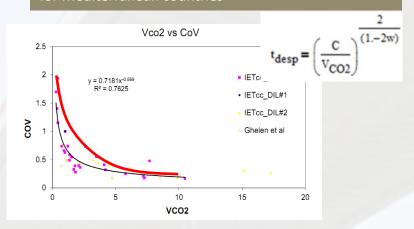
$$V_{corr_d} = \mu_{Vcorr} - \begin{pmatrix} 0.70 \\ 0.30 \end{pmatrix} \cdot \beta \cdot CoV$$

Expossure	V _{corr} [μm/y]	CoV (%)	V _{corr,D} β=1,5	Tpr[yr] β=1,5	t _{ini,D} β=1,5
XC1	1	65	2.0	25	25
XC2	4	65	5.4	9	41
XC3	2	65	4.0	13	37
XC4	5	90	12.9	4	46
XS1	30	60	56.3	1	49
XS2	10	60	13.1	4	46
XS3	70	90	105.0	0	50

Only some exposure cases merit a calculation of propagation time $t_{\rm p}$, in other cases propagation time is negligible.

- Cover calculation for tables
 - Carbonation

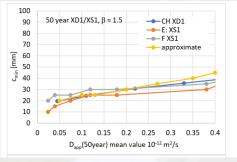
Calculated values for XC3 & XC4 are provided for RH = 75%, which may correspond to Central Europe but not for Mediterranean countries

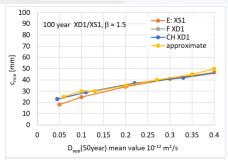


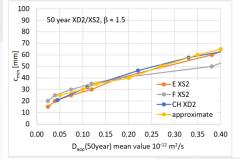
Relation average carbonation rate and 90% fractile is computed using following eq.

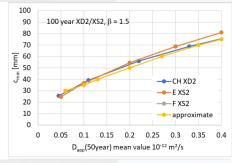
Chlorides

$$t_{dep} = \left(\frac{C - \Delta x}{V_{cl}(t)}\right)^{\frac{2}{1-n}}$$

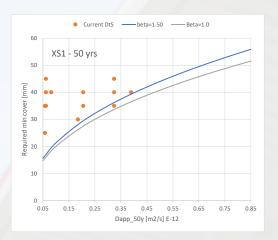


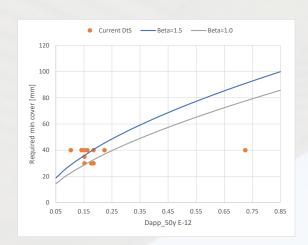


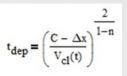


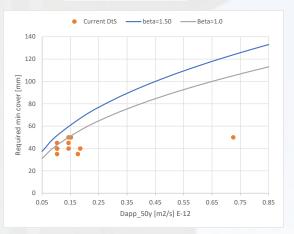


- Cover calculation for tables
 - Chloride induced corrosion









With current proposal, durable concrete should not be achieved using CEMI cement in XS/XD2 & XS/XD3

- Minimum cover provided tables
 - Provided as NDP
 - Calibrated for 50 and 100 yrs, including 50μm/ 500μm rebar corrosion
 - Calibrated for HR = 75% (XC3/XC4), values for Mediterranean Countries may differ
 - a priori deviations for the 90% fractile calculations
 - Additional allowance for different construction tolerances (NDP)

