

# INVITED CONFERENCE

## Anchorage and laps of reinforcing steel

John Cairns



EUROCODES

EN 1992

Design  
of concrete  
structures

### 2<sup>nd</sup> generation of Eurocode 2 on concrete structures

Madrid, October 17<sup>th</sup>, 2023



## **FprEC2:2023 Sections 11.3 & 11.4**

1. Some basics of bond behaviour
2. Calculation of anchorage length, straight bars in tension
3. Hooks, bends, U loops
4. Laps of bars in tension
5. Compression laps and anchorages
6. New content: Post-installed reinforcement, headed bars
7. Impact on design

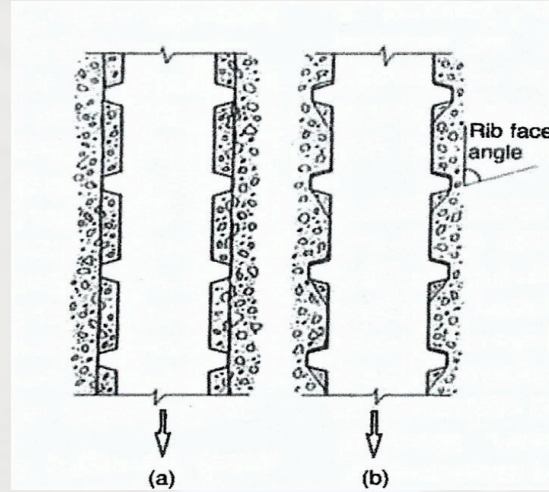
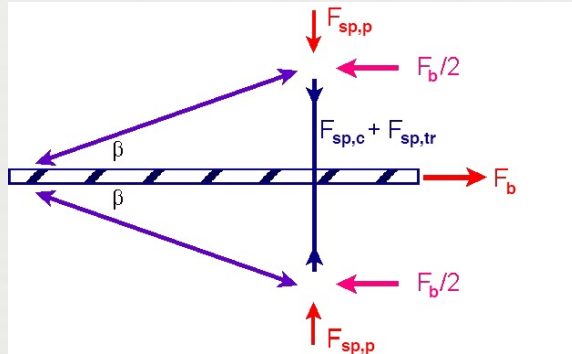
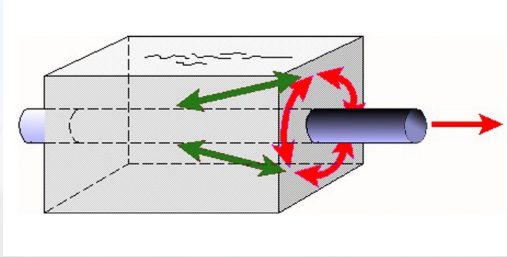
### **Aims:**

Describe change, explain rationale, quantify impact.



## I.1 Some basics of bond behaviour

### Splitting and pull-out modes



Shearing over  
tops of  
deformations

**Non-  
ductile**

Bearing of  
deformations,  
splitting

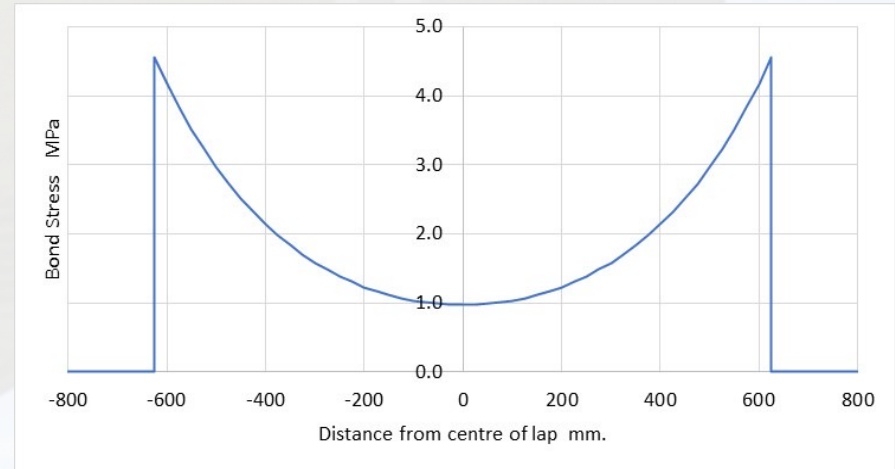
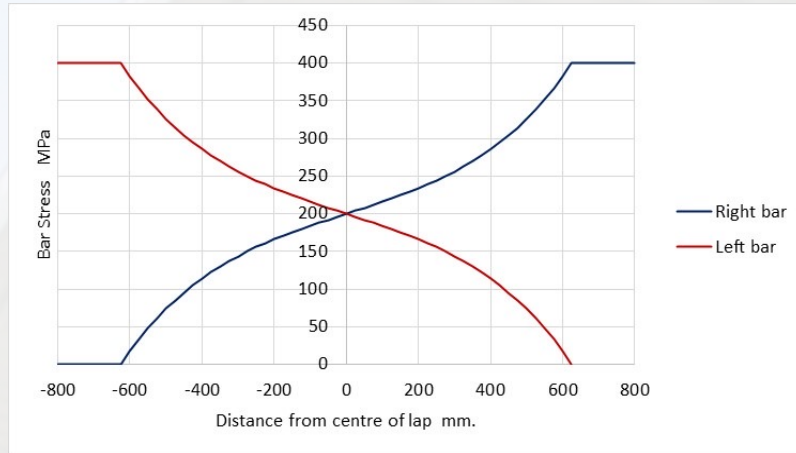
**Brittle**



## 1.2 Some basics of bond behaviour

Variation in stress over bond length is non-linear

Pair of lapped bars,  $\phi = 25\text{mm}$ ,  $l_b = 50\phi$ ,  $\sigma_{sd} = 400\text{MPa}$



Bar stresses

(Plots based on linear elastic analysis  
using MC local bond-slip relationship)

Bond stresses



# Principal sources

## EC2:2004

Based on CEB-FIP  
Model Code 1978,  
(with some modifications)

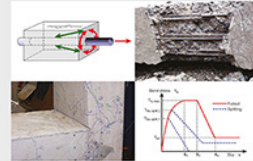
## FprEC2:2023

2014  
Bulletin 72 Background

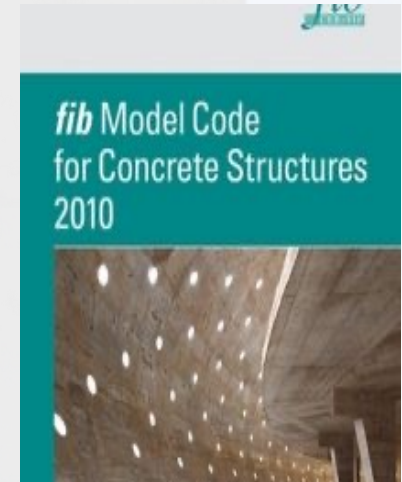
2013  
MC2010 Sect. 6.1

Bulletin 72

technical report



Bond and anchorage of  
embedded reinforcement:  
Background to the *fib*  
Model Code for Concrete  
Structures 2010



## 2.1 Calculation of anchorage lengths, straight bars

### EC2:2004

$$f_{bd} = 2,25 \eta_1 \eta_2 f_{ctd}$$

$$l_{b,rqd} = (\phi / 4) (\sigma_{sd} / f_{bd})$$

$$l_{bd} = \alpha_1 \alpha_2 \alpha_3 \alpha_4 \alpha_5 l_{b,rqd} \geq l_{b,min}$$

$\eta_1, \eta_2$  bar size, casting position

$\alpha$ : hook/bend, min. cover, transverse compression

Influencing parameters multiplicative

### FprEC2:2023 : simplified provisions

Table 11.1 (NDP) — Anchorage length of straight bars divi

$\phi$ [mm]	Anchorage length $l_{bd}/\phi$				
	$f_{ck}$				
	20	25	30	35	40
$\leq 12$	47	42	38	36	33
14	50	44	41	38	35
16	52	46	42	39	37
20	56	50	46	42	40
25	60	54	49	46	43

**Simplified provision** for ribbed bars  $\phi \leq 32$  mm, indented bars  $\phi \leq 14$  mm,  $c_d \geq 1,5\phi$ ,  $\sigma_{sd} = 435$  MPa, good bond conditions

## 2.2 Calculation of anchorage lengths, straight bars :detailed provisions

### FprEC2:2023 : detailed provisions

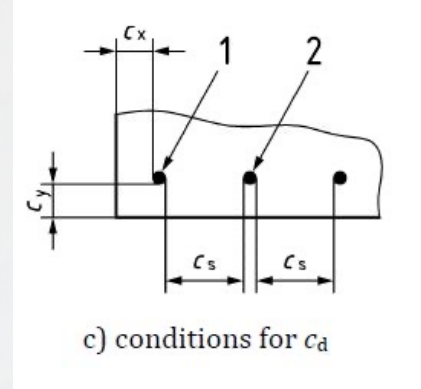
$$l_{bd} = k_{lb} \cdot k_{cp} \cdot \phi \cdot \left( \frac{\sigma_{sd}}{435} \right)^{n_\sigma} \cdot \left( \frac{25}{f_{ck}} \right)^{\frac{1}{2}} \cdot \left( \frac{\phi}{20} \right)^{\frac{1}{3}} \cdot \left( \frac{1,5\phi}{c_{d,conf}} \right)^{\frac{1}{2}} \geq 10\phi \quad (11.3)$$

$$c_d = \min\{0,5c_s; c_x; c_y; 3,75\phi\}$$

$$(\phi/20 \text{ mm}) \geq 0,6 \text{ and } (25/f_{ck}) \geq 0,3$$

$$c_{d,conf} = \min\left\{c_x; c_y + 25 \frac{\phi_t^2}{s_t}; \frac{c_s}{2}; 3,75\phi\right\} + \Delta c_d \leq 6\phi \quad (11.4)$$

$$\Delta c_d = (70\rho_{conf} + 12\sigma_{ccd}/\sqrt{f_{ck}})\phi;$$



Where transverse compression or an appreciable quantity of secondary reinforcement restrain splitting failure

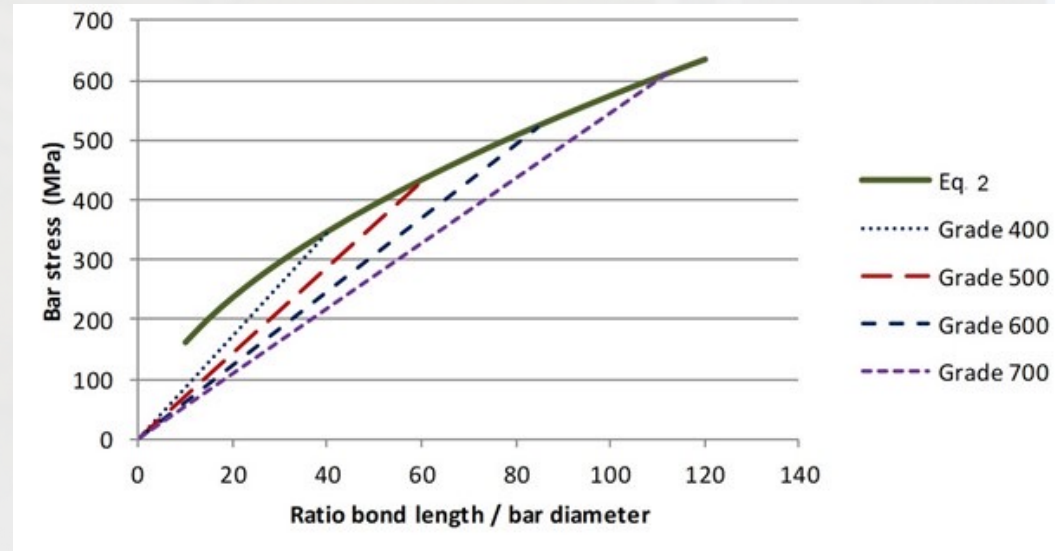
Confinement parameters summative

## 2.2a Bond length and elimination of ultimate bond strength

$$f_{stm} = 54 \left( \frac{f_{cm}}{25} \right)^{0.25} \left( \frac{l_b}{\phi} \right)^{0.55} \left( \frac{25}{\phi} \right)^{0.2} \left[ \left( \frac{c_{min}}{\phi} \right)^{0.25} \left( \frac{c_{max}}{c_{min}} \right)^{0.1} + k_m K_{tr} \right] \quad \text{Eq 2}$$

Eq 2 mean anchorage strength expression, from fib Bulletin 72

Gradient of straight lines represents average bond stress



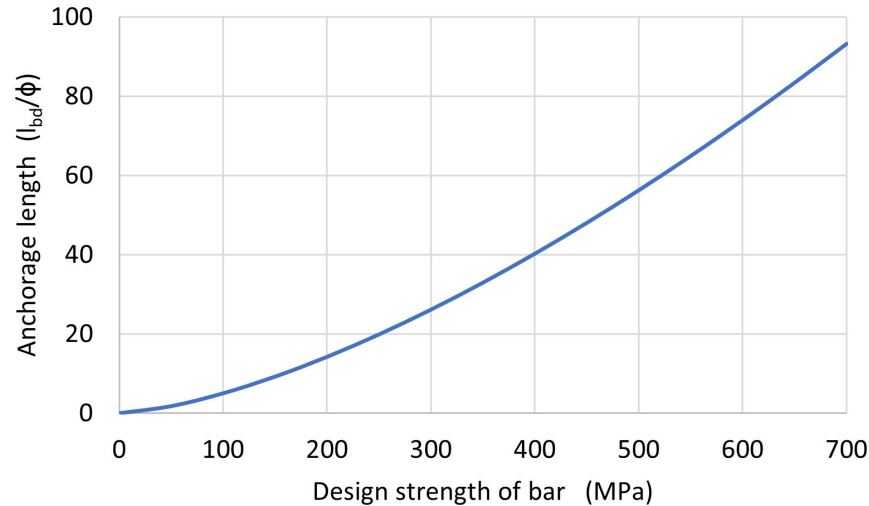


## 2.2b Influence of design strength of bar

$$l_{bd} = k_{lb} \cdot k_{cp} \cdot \phi \cdot \left( \frac{\sigma_{sd}}{435} \right)^{n_{\sigma}} \cdot \left( \frac{25}{f_{ck}} \right)^{\frac{1}{2}} \cdot \left( \frac{\phi}{20} \right)^{\frac{1}{3}} \cdot \left( \frac{1,5\phi}{c_d} \right)^{\frac{1}{2}} \geq 10\phi \quad (11.3)$$

$$n_{\sigma} = 1.5$$

*Non-linear  
influence of  
bond length*



$$\begin{aligned} f_{ck} &= 30\text{MPa} \\ \phi &= 20\text{mm} \\ c_d &= 30\text{mm} \end{aligned}$$

## 2.3 Influence of concrete strength

### EC2:2004

$$f_{bd} = 2,25 \eta_1 \eta_2 f_{ctd}$$

Tensile strength of concrete

$$f_{ctd} = f_n(f_{ck})^{0.67}$$

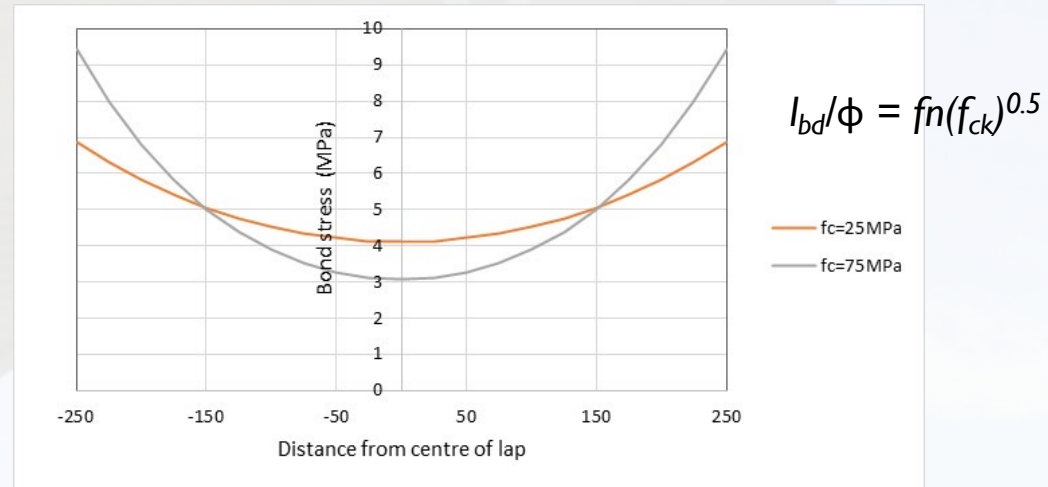
=>

$$l_{bd}/\phi = f_n(f_{ck})^{0.67}$$

Valid only for  
short bond  
lengths

### FprEC2:2023

$$l_{bd} = k_{lb} \cdot k_{cp} \cdot \phi \cdot \left(\frac{\sigma_{sd}}{435}\right)^{n_\sigma} \cdot \left(\frac{25}{f_{ck}}\right)^{\frac{1}{2}} \cdot \left(\frac{\phi}{20}\right)^{\frac{1}{3}} \cdot \left(\frac{1,5\phi}{c_d}\right)^{\frac{1}{2}} \geq 10\phi$$



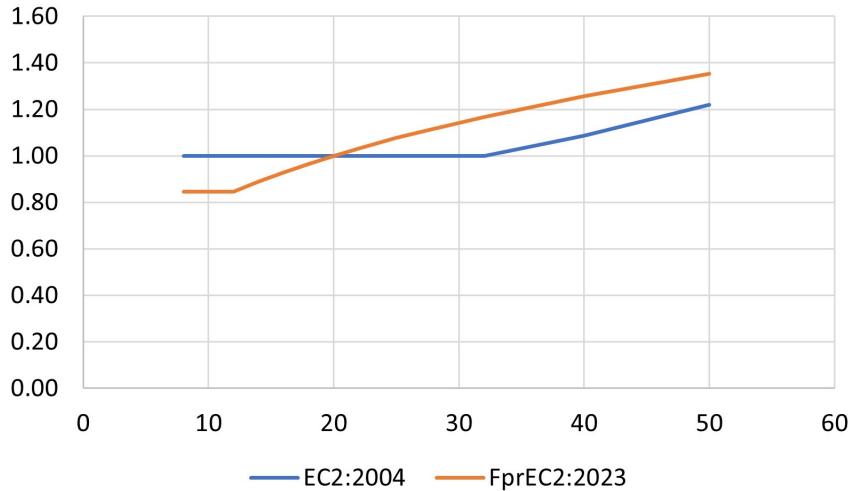
Pair of lapped bars,  $\phi = 25\text{mm}$ ,  $l_b = 20\phi$ ,  $\sigma_s = 400\text{MPa}$

## 2.4 Influence of bar size

### EC2:2004

$\eta_2 = 1,0$  for  $\phi \leq 32$  mm

$\eta_2 = (132 - \phi)/100$  for  $\phi > 32$  mm



### FprEC2:2023

$$l_{bd} = k_{lb} \cdot k_{cp} \cdot \phi \cdot \left(\frac{\sigma_{sd}}{435}\right)^{n_{\sigma}} \cdot \left(\frac{25}{f_{ck}}\right)^{\frac{1}{2}} \cdot \left(\frac{\phi}{20}\right)^{\frac{1}{3}} \cdot \left(\frac{1,5\phi}{c_d}\right)^{\frac{1}{2}} \geq 10\phi$$

$\phi/20 \geq 0.6$  based on test data  
and lower rib area required for  
bars <12mm:

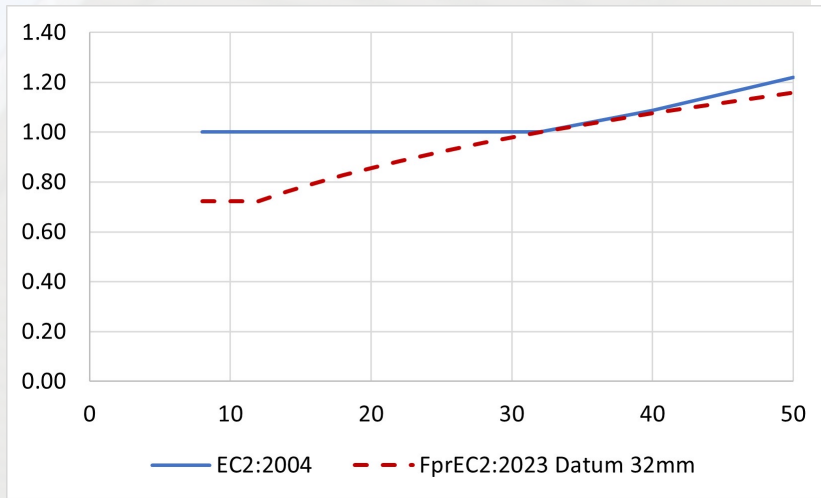
Value of function for bar size

## 2.4 Influence of bar size

### EC2:2004

$\eta_2 = 1,0$  for  $\phi \leq 32$  mm

$\eta_2 = (132 - \phi)/100$  for  $\phi > 32$  mm



### FprEC2:2023

$$l_{bd} = k_{lb} \cdot k_{cp} \cdot \phi \cdot \left(\frac{\sigma_{sd}}{435}\right)^{n_{\sigma}} \cdot \left(\frac{25}{f_{ck}}\right)^{\frac{1}{2}} \cdot \left(\frac{\phi}{20}\right)^{\frac{1}{3}} \cdot \left(\frac{1,5\phi}{c_d}\right)^{\frac{1}{2}} \geq 10\phi$$

$\phi/20 \geq 0.6$  based on test data  
and lower rib area required for  
bars <12mm:

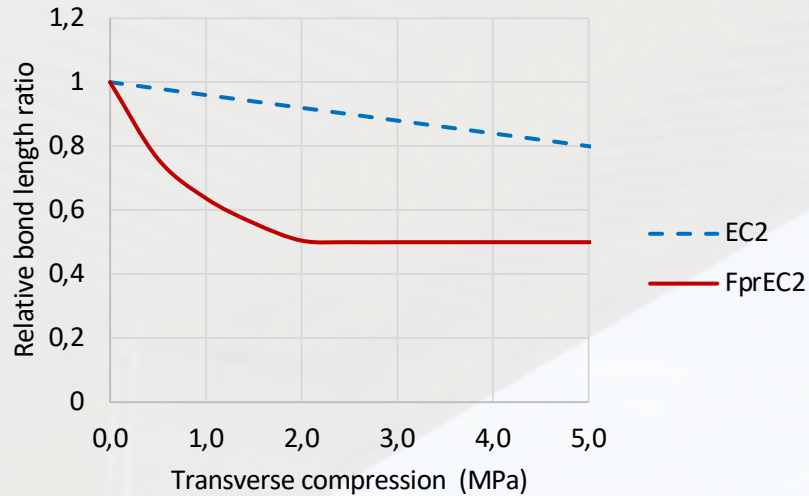
Influence on bond length, rebased  
to common datum (32mm)



## 2.5 Influence of transverse compression

### EC2:2004

$$\alpha_5 = 1,0 - 0,04p$$
$$0,7 \leq \alpha_5 \leq 1,0$$



### FprEC2:2023

$$\Delta c_d = (70\rho_{\text{conf}} + 12\sigma_{\text{ccd}}/\sqrt{f_{\text{ck}}})\phi;$$

(FprEC2 relative bond length dependent on other contributions to confinement)

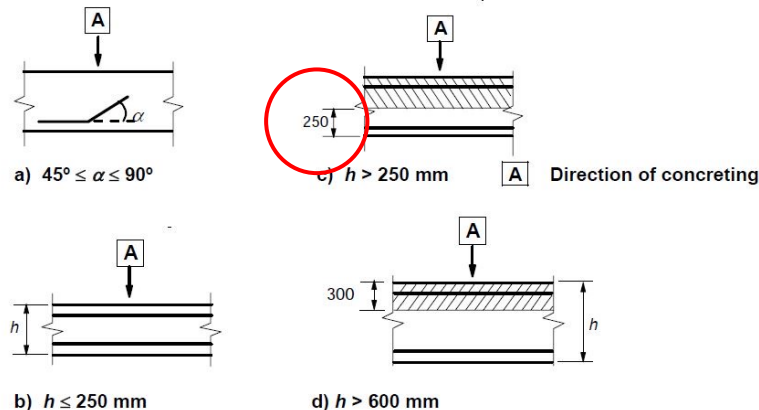
## 2.6 Casting position (bars $< 45^\circ$ to horizontal)

### EC2:2004

Coefficient  $\eta_1$  applied to bond strength:

$\eta_1 = 1.0$  and  $0.7$  for good and poor bond conditions respectively.

Equivalent to **43%** greater bond lengths for poor condition



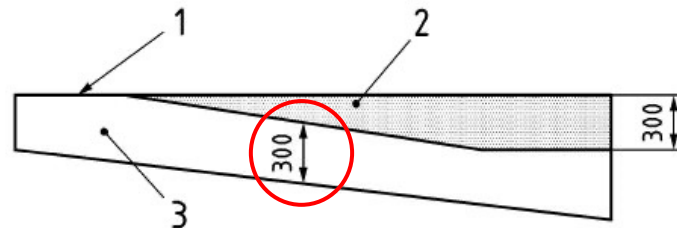
### FprEC2:2023

Coefficient  $k_{cp}$  applied to bond length:

$k_{cp} = 1.0$  for good bond conditions

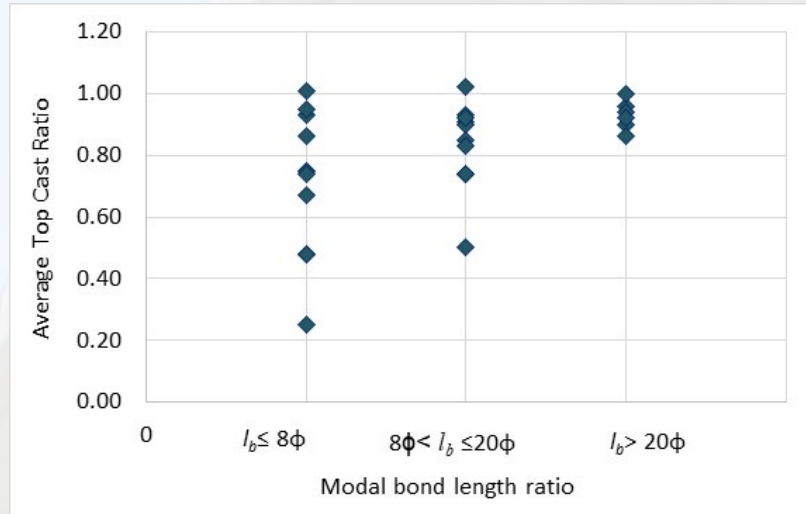
$k_{cp} = \mathbf{1.2}$  for poor bond conditions

$k_{cp} = 1.4$  under bentonite or similar



## 2.6a Casting position

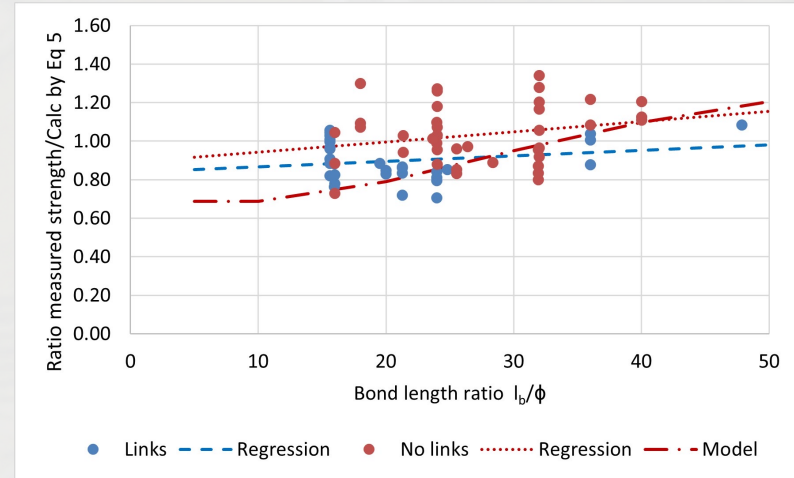
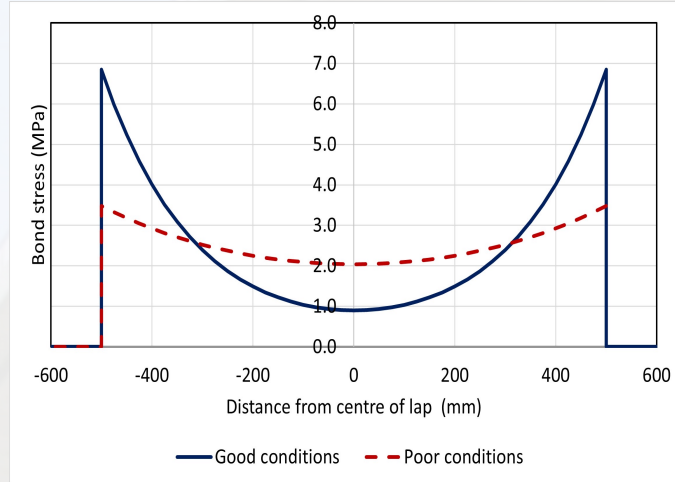
Top cast ratio = maximum stress anchored in bar cast near top of pour/ that in bar cast near the bottom



Wide range reported

## 2.6b Casting position

### Analysis of distribution of bond stress through lap using MC2010 local bond-slip model



*Over practical bond lengths, more uniform distribution of bond stress through a 'top cast' lap partially compensates for weaker bond strength in a 'poor' casting position*



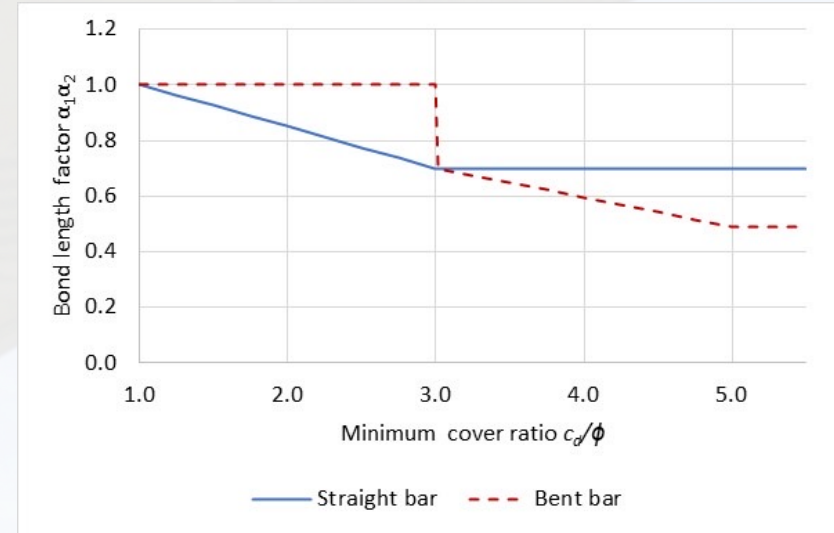
### 3 Contribution of end hooks and bends to tension anchorages

#### EC2:2004

Influencing factor	Type of anchorage	Reinforcement bar	
		In tension	I
Shape of bars	Straight	$\alpha_1 = 1,0$	
	Other than straight (see Figure 8.1 (b), (c) and (d))	$\alpha_1 = 0,7$ if $c_d > 3\phi$ otherwise $\alpha_1 = 1,0$ (see Figure 8.3 for values of $c_d$ )	

30% reduction in anchorage length for hook  
or bend, provided  $c_d/\phi > 3.0$

- Contribution of a bend increases with stress to be anchored
- No reduction in  $l_{bd}$  for  $c_d \leq 3\phi$



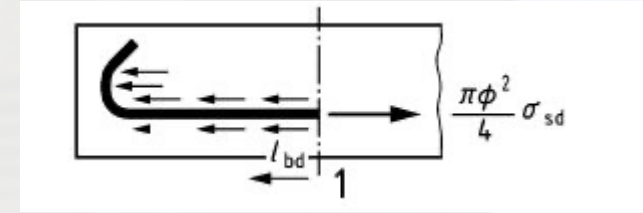
### 3b Contribution of end hooks and bends to tension anchorages

#### EC2:2004

Influencing factor	Type of anchorage	Reinforcement bar	
		In tension	I
Shape of bars	Straight	$\alpha_1 = 1,0$	
	Other than straight (see Figure 8.1 (b), (c) and (d))	$\alpha_1 = 0,7$ if $c_d > 3\phi$ otherwise $\alpha_1 = 1,0$ (see Figure 8.3 for values of $c_d$ )	

30% reduction in anchorage length for hook  
or bend, provided  $c_d/\phi > 3.0$

#### FprEC2:2023



The design anchorage length may be reduced by:

15 $\phi$  for standard hooks and bends  
20 $\phi$  for U-loops

## 4 Tension laps, straight bars

### EC2:2004

Percentage of lapped bars relative to the total cross-section area	< 25%	33%	50%	>50%
$\alpha_6$	1	1,15	1,4	1,5
<b>Note:</b> Intermediate values may be determined by interpolation.				

$$l_0 = \alpha_1 \alpha_2 \alpha_3 \alpha_5 \alpha_6 l_{b,rqd} \geq l_{0,min}$$

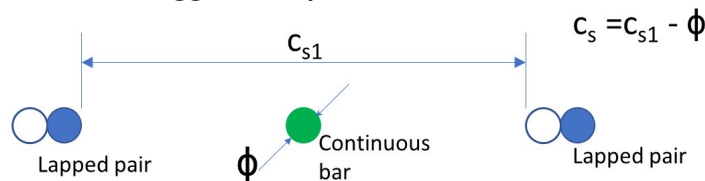
Rules similar to anchorages but with factor  $\alpha_6$  dependent on percentage bars lapped at section

### FprEC2:2023

$$k_{ls} = 1,2$$

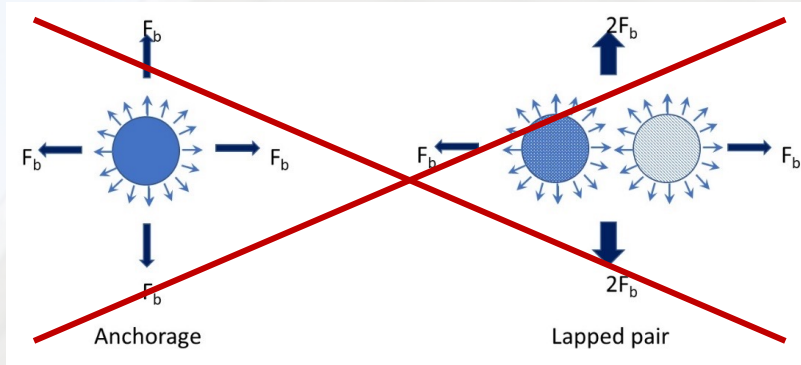
Rules similar to anchorages but with factor  $k_{ls} = 1,2$  (NDP) independent of percentage bars lapped at section

Clarification of bar spacing dimension for staggered laps



## 4.1 Tension laps, straight bars

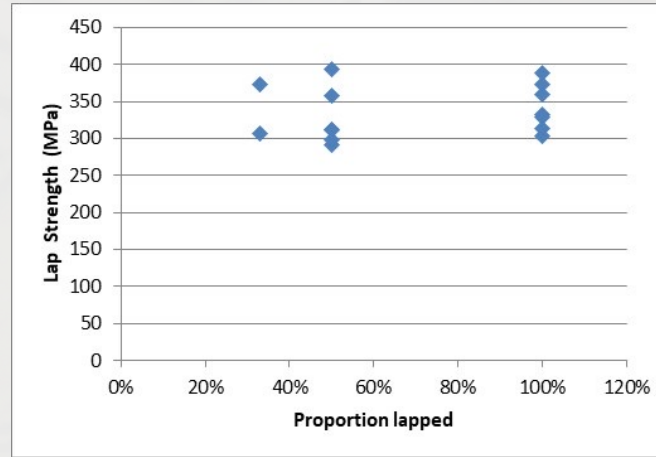
1975: Hydraulic pressure analogy laps vs. anchorages



Laps produce double the splitting of anchorages

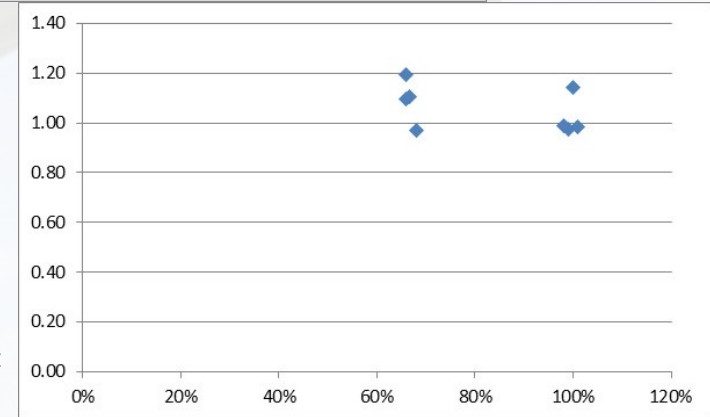
$\alpha_6$  factor in EC2:2004 inconsistent with test results

Test evidence



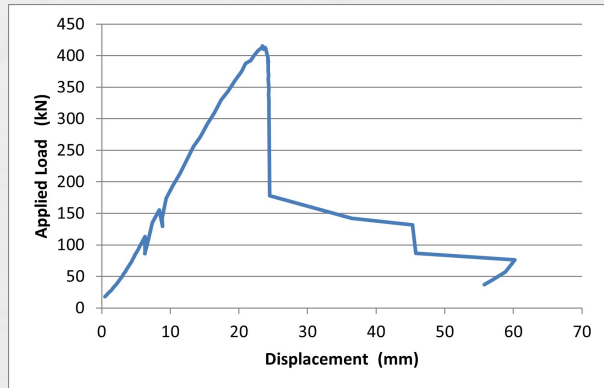
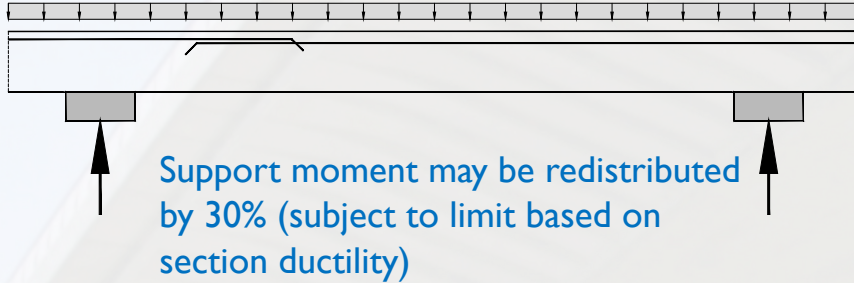
Cairns 2014

Thompson Jirsa  
Breen Meinheit  
1975



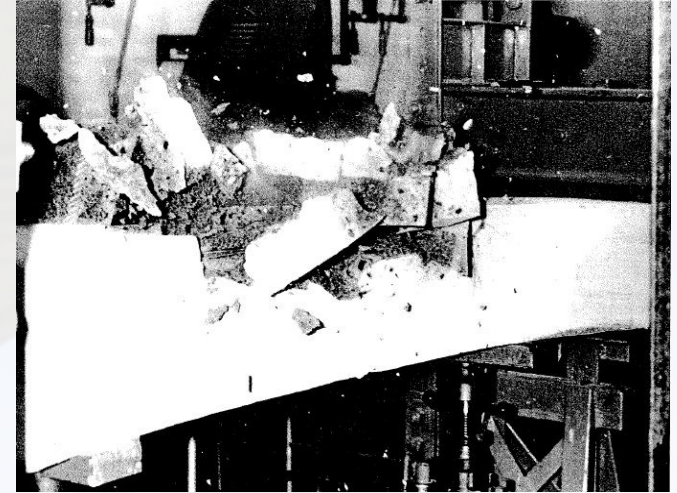


## 4.2 Tension laps, robustness



>50% strength loss immediately after peak load

### Explosive failure of lap, Tepfers 1974

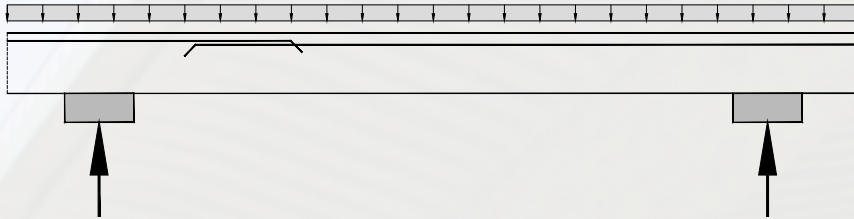


Locate laps away from areas of high bar stress wherever possible

## 4.2a Tension laps, robustness

### EC2:2004

No specific requirements



### FprEC2:2023

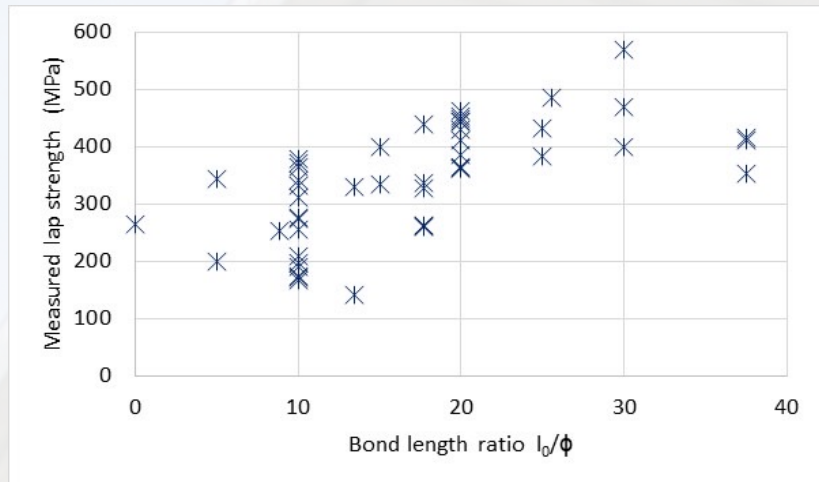
Additional requirements for laps in vicinity of plastic hinges/ yield lines :

- additional confining reinforcement provided
- area lapped  $\leq 35\%$

Alternatively

- Design for  $1,2 \sigma_{sd}$

## 5 Compression laps and anchorages



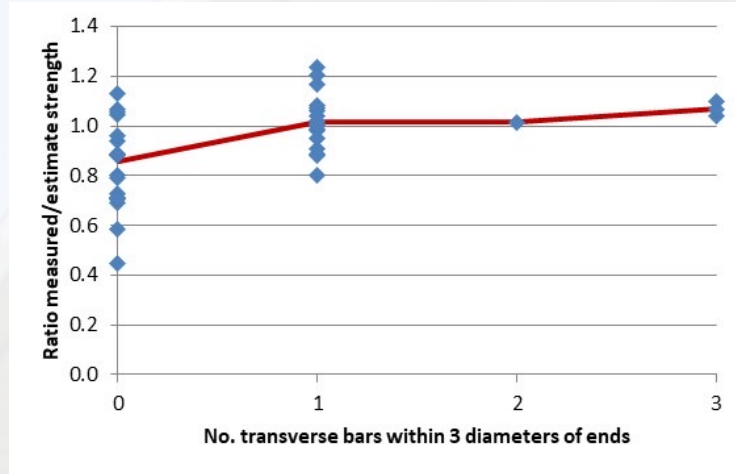
Strength of compression laps, all test results

### FprEC2:2023

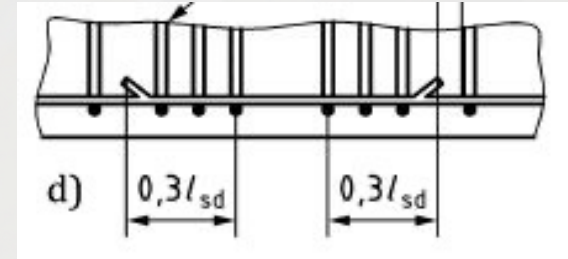
Expressions 11.3 and 11.4 as for bars in tension

Design anchorage length may be reduced by  $15\phi$  provided requirements for detailing of links near ends of laps are satisfied

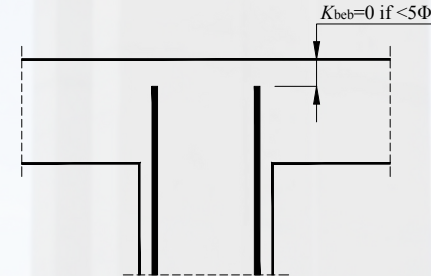
## 5b Compression laps and anchorages



Weaker anchorage if no links near ends



Confining reinforcement to be located close to ends of compression laps



No allowance for bars ending near a face



## 6 New content

### Bonded post-installed reinforcing steel

Broadly consistent with cast-in, but additional requirements on anchoring mortar, cover.

Additional restrictions on concrete grade,  $\sigma_{sd}$



### Headed bars

Head can provide full anchorage for Grade 500 bars if specified conditions of cover, spacing, head geometry, concrete strength are satisfied.

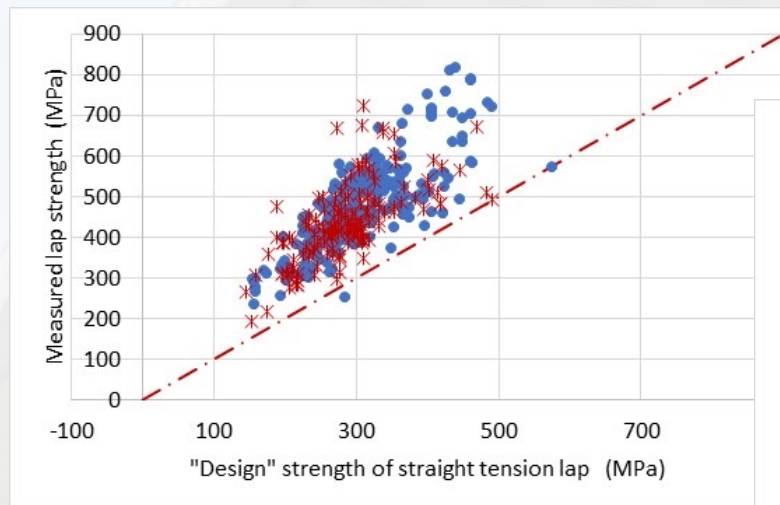
Detailed provisions for head capacity in other circumstances

Additional 10% on bond length where head and straight length of bar act in combination

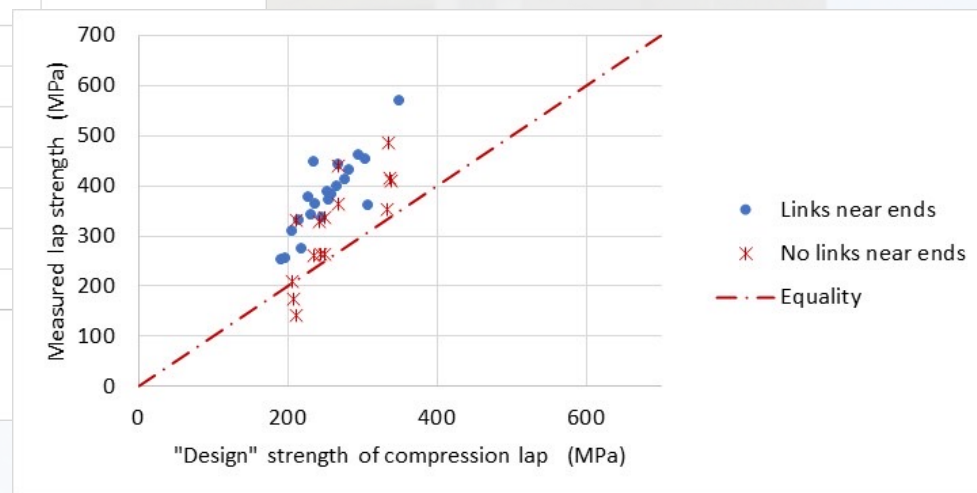


## 7 Impact on design

FprEC2:2023 provisions validated against extensive sets of data



Tension laps



Compression laps

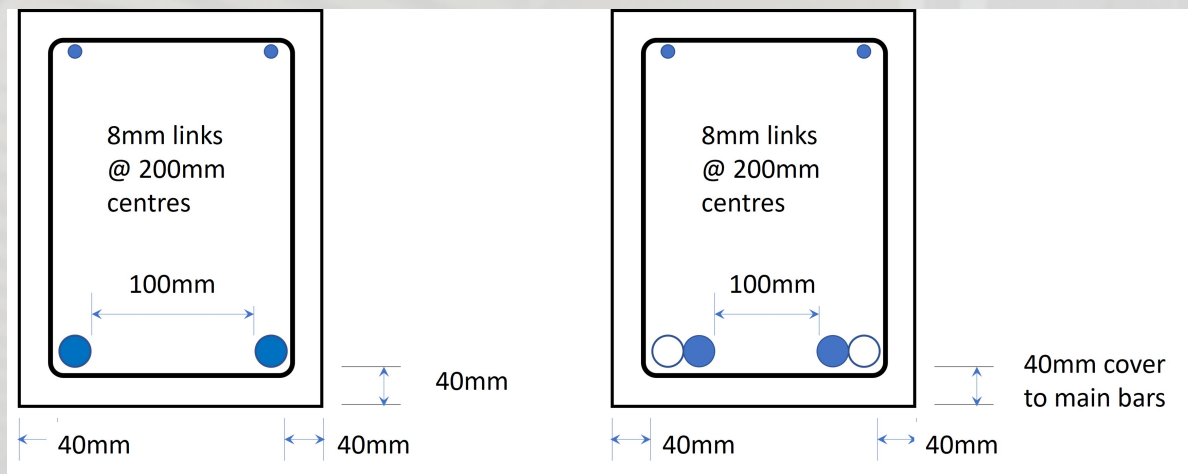
## 7 Impact on design

### Sample sections

Bar sizes 12 and 25 ( $c_d/\phi$  3.33 and 1.6)

Concrete strength  $f_{ck}$  25MPa and 60MPa

Design for  $\sigma_{sd} = 435$  MPa



$$c_d = 40\text{mm}$$

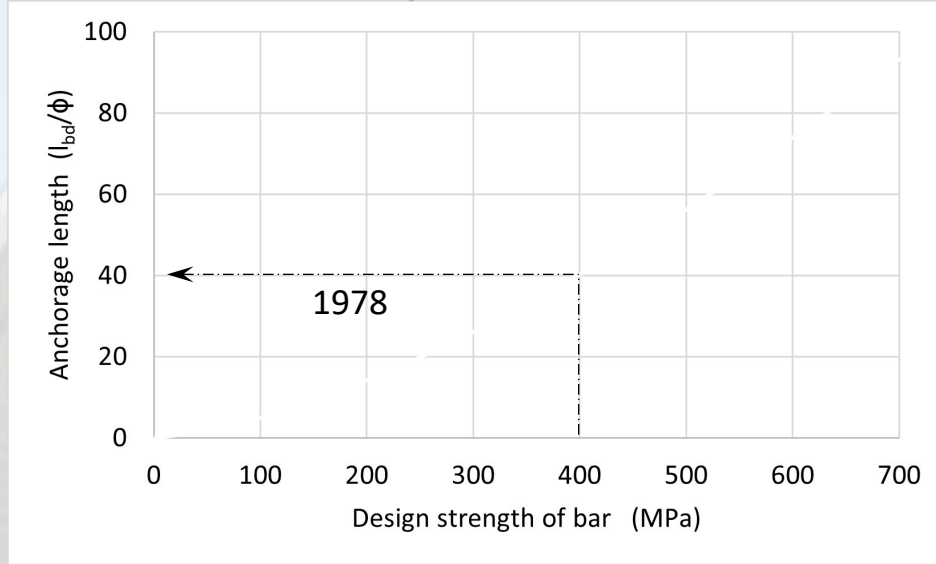
Anchorage

Lap



## 7.1 Impact on design

### Evolution of bar strength

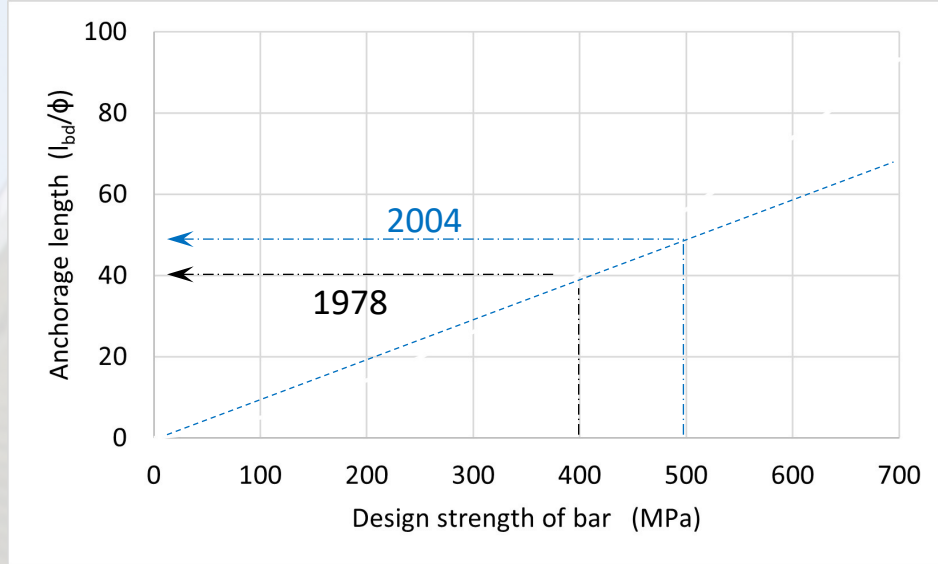


1978 :  $f_{yk} \sim 400\text{MPa}$

Say bond length corresponds to  $40\phi$



## 7.1 Impact on design

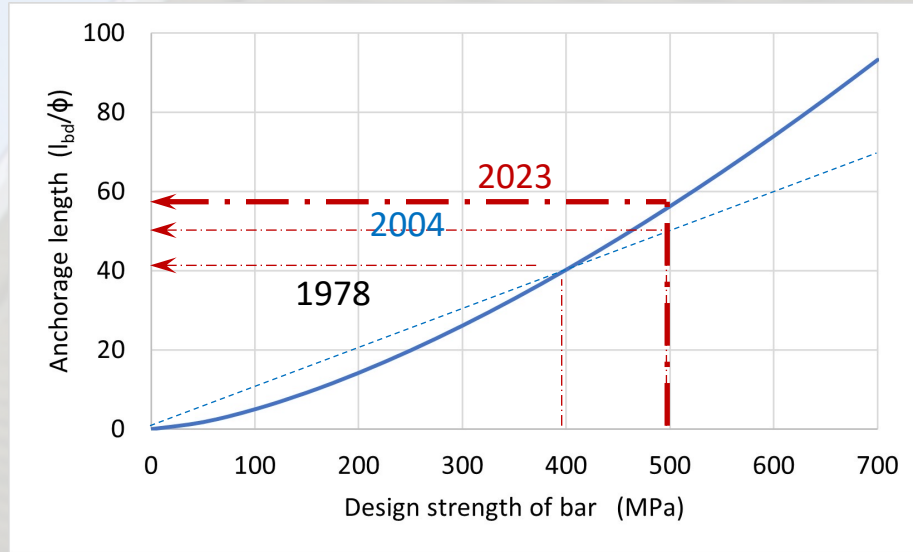


1978 :  $f_{yk} \sim 400\text{MPa}$

$f_{yk}$  now  $\sim 500\text{MPa}$

EC2:2004 provisions  $\Rightarrow l_{bd} = 50 \phi$   
a +25% increase

## 7.1 Impact on design



1978 :  $f_{yk} \sim 400\text{MPa}$

$f_{yk}$  increased to  $\sim 500\text{MPa}$

EC2:2004 provisions  $\Rightarrow l_{bd} = 50 \phi$

a +25% increase

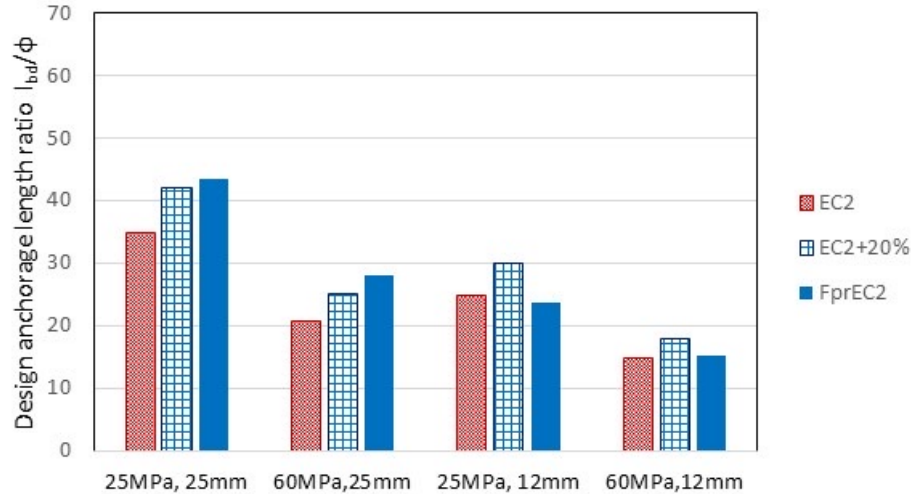
But allowing for non-linear behaviour

$\Rightarrow l_{bd} = 55.9\phi$

i.e. 12% greater increase

MC2020 indicates 20% increase

## 7.2a Impact on design



Anchorage, good casting position

*Longer anchorage lengths for larger bars*



EC2 : design bond length according to EC2:2004, the current EuroCode

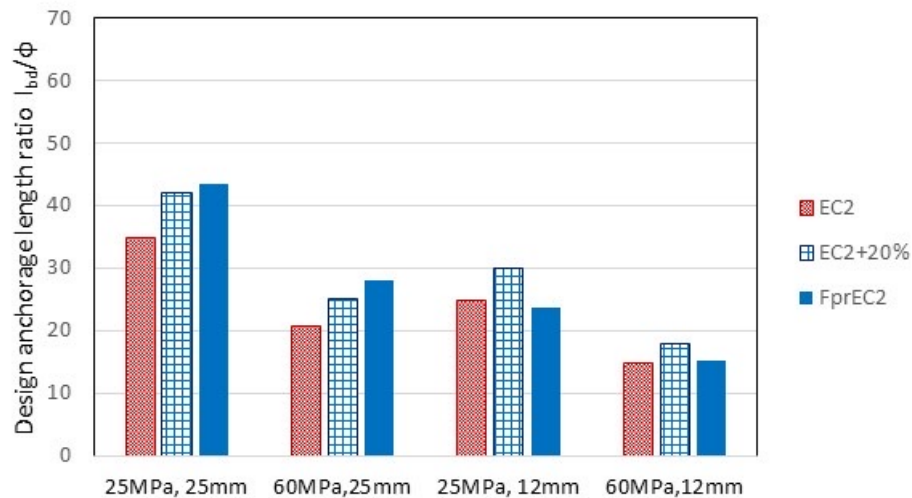


EC2+20% : design bond length according to EC2:2004 with correction for steel strength



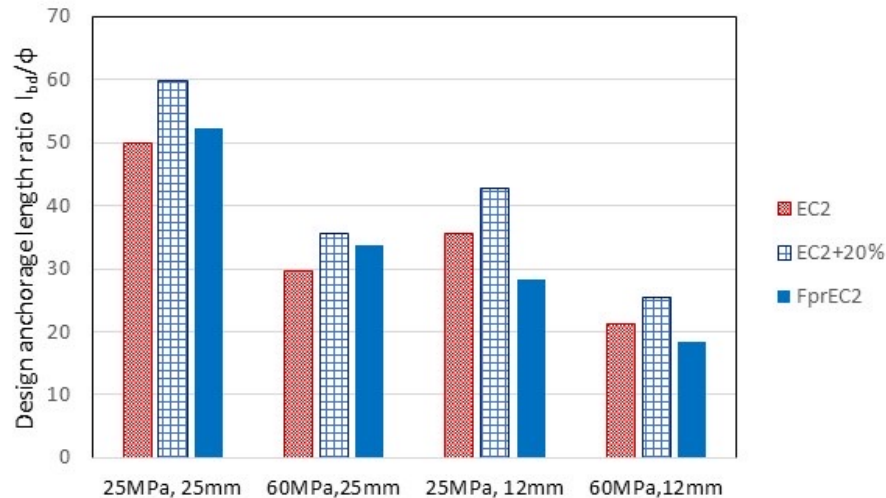
FprEC2 : design bond length according to FprEC2:2023, the revised EC

## 7.2a Impact on design



Anchorage, good casting position

*Longer anchorage lengths for larger bars*

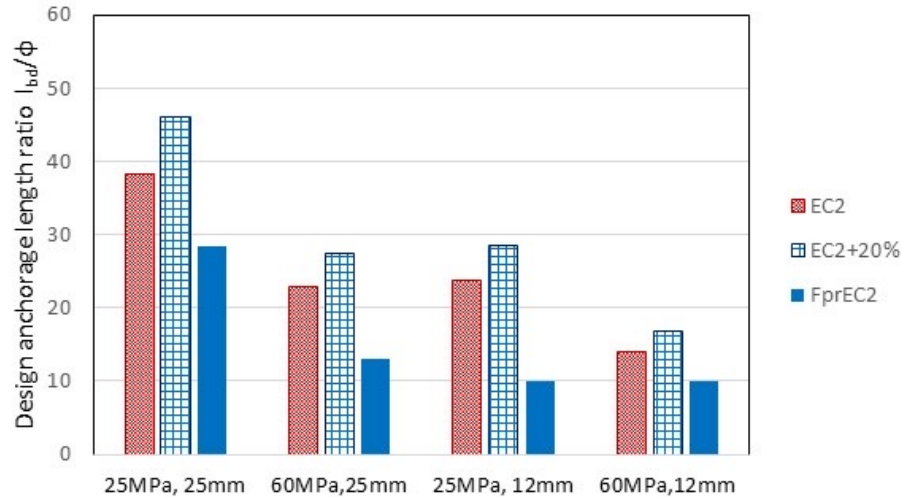


Anchorage, poor casting position

*Little difference larger bars, shorter small bars*

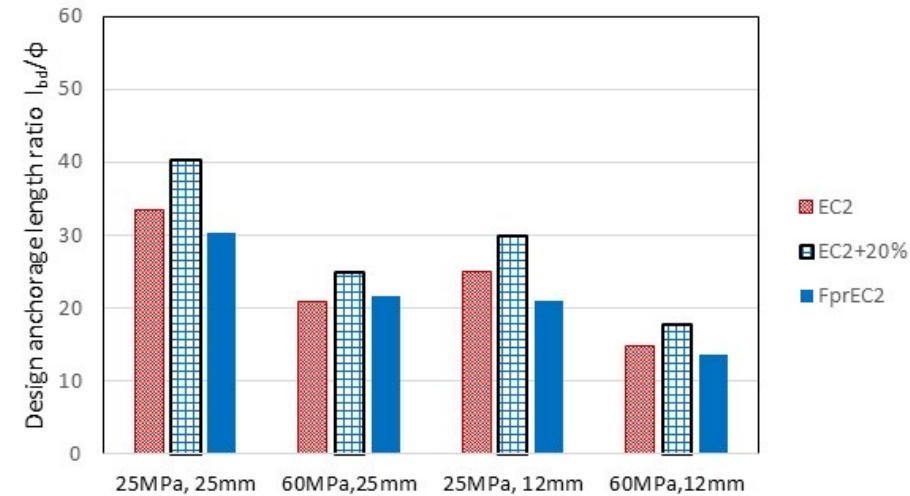


## 7.2b Impact on design



Hook/bent bar, good casting position

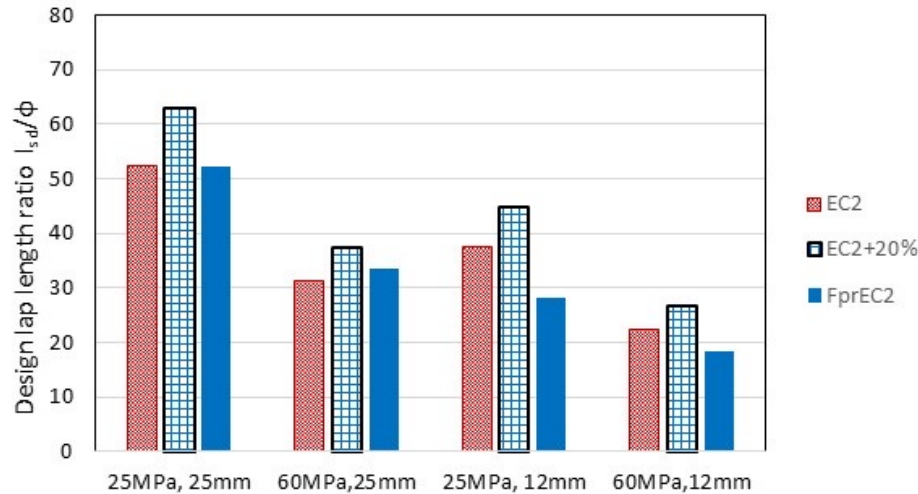
*Shorter anchorage lengths*



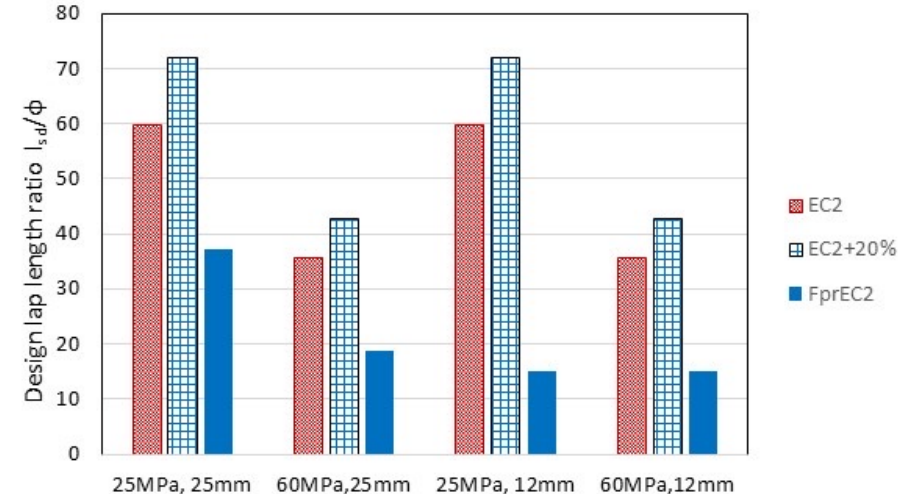
Anchorage subject to 1.0 MPa transverse compression, good casting position

*Shorter anchorage lengths*

## 7.2c Impact on design



Tension lap, good casting position, 100% lapped  
*Generally slightly shorter lap lengths*



Compression lap, good casting position  
*Considerably shorter lap lengths*

## Summary

1. Extensive revision of section on anchorage and laps of reinforcing steel in FprEC2:2023
2. *fib* Bulletin 72 has formed the basis for many of the revised provisions
3. 'Bond strength' eliminated, non-linear variation in capacity with bond length recognized, hence bond lengths now calculated directly
4. Look-up table for routine situations, detailed expressions account for greater (or lesser) confinement from cover, transverse reinforcement or transverse pressure
5. Hooks/bends contribute an equivalent straight bond length, reduced influence of poor casting position, etc.
6. Compression laps/anchorage treated in a more consistent and rational manner
7. New content on PIR, headed bars, assessment
8. Typically modest increase in design anchorage lengths of larger size straight bars, reductions for bent/hooked bars or U-loops, bars in compression





**Thank you for your attention**

John Cairns